

# BLADE STRUCTURE IN A GAS TURBINE

## FIELD OF THE INVENTION

This invention relates to a blade structure in a gas turbine. More particularly, this invention relates to a blade structure of a gas turbine with improved turbine efficiency by restricting pressure loss to a minimum level.

## BACKGROUND OF THE INVENTION

10 A gas turbine will be explained with reference to Fig. 16. In general, a gas turbine is equipped with a plurality of stages of stationary blades 2 and 3 arrayed in a circle on a casing (a blade circle or a vehicle chamber) 1, and a plurality of moving blades 5 arrayed in a circle on a rotor (a hub of a base) 4. Fig. 16 shows the moving blade 5 at 15 a certain stage, the stationary blade 2 at the same stage (the inlet side of combustion gas 6) as this moving blade 5, and the stationary blade 3 at the next stage (the outlet side of the combustion gas 6) of this moving blade 5.

20 When pressure loss is large in the gas turbine, turbine efficiency is lowered. Therefore, it is important to improve the turbine efficiency by minimizing the pressure loss.

However, as shown in Fig. 16, there is a case where 25 the moving blade 5 at a certain stage is what is called a

free-standing moving blade that has a clearance 8 between a chip 7 of this moving blade 5 and the casing 1. In the case of this free-standing moving blade 5, there is the following problem.

5 . Namely, as shown in Fig. 17, a main flow (shown by a solid-line arrow mark in Fig. 17) of combustion gas 6 flows to the next-stage stationary blade 3 side by passing through between the moving blade 5 and the moving blade 5. In the mean time, in the clearance 8 between the chip 7 of the moving  
10 blade 5 and the casing 1, there is generated a leakage flow 9 (shown by a broken-line arrow mark in Fig. 17) that is separate from the main flow of the combustion gas 6.

A mechanism of generating the leakage flow 9 is that as the pressure at a belly surface 10 side of the moving  
15 blade 5 is higher than the pressure at a rear surface 11 side of the moving blade 5, the leakage flow 9 is generated from the belly surface 10 side to the rear surface 11 side based on a difference between these pressures.

As shown in Fig. 17, the leakage flow 9 flows at an  
20 incidence angle  $i_c$  to the rear surface 13 side at a front edge 12 of the chip of the stationary blade 3 at the next stage. This leakage flow 9 becomes a flow opposite to the main flow of the combustion gas 6 that flows to the belly surface 14 side of the stationary blade 3.

25 Therefore, a vortex flow 15 (shown by a solid-line

spiral arrow mark in Fig. 17) is generated at the belly surface 14 side of the front edge 12 of the chip of the stationary blade 3. When this vortex flow 15 is generated, pressure loss occurs. The main flow of the combustion gas 6 may deviate from the belly surface 14 side of the stationary blade 3. In Fig. 17, a reference symbol  $\beta_c$  denotes an entrance metal angle at the chip portion of the stationary blade 3. Similarly, a reference symbol  $\theta_c$  denotes a front-edge including angle at the chip portion of the stationary blade 3. Similarly, a reference number 22 denotes a camber line for connecting between the front edge 12 of the chip portion of the stationary blade 3 and a rear edge 23 of the chip portion.

The incidence angle  $i_c$  of the leakage flow 9 and the pressure loss have a relative relationship as shown by a solid-line curve in Fig. 18. The solid-line curve in Fig. 18 shows a case of the front-edge including angle  $\theta_c$  at the chip portion of the stationary blade 3 shown in Fig. 17.

In this case, the front-edge including angle  $\theta_c$  at the chip portion of the stationary blade 3 has been set such that the pressure loss becomes minimum (refer to a point P1 in Fig. 18). However, as described above, the leakage flow 9 is generated, and the pressure loss also becomes large when the incidence angle  $i_c$  of this leakage flow 9 is large (refer to a point P2 in Fig. 18). When this pressure loss

is large, the turbine efficiency is lowered by that amount.

Further, as shown in Fig. 16, seal-air 16 (shown by a two-dot chained line arrow mark in Fig. 16) flows from the rotor 4 side at the upstream of the moving blade 5 at a certain stage. When this seal-air 16 is flowing, there is the following problem.

Namely, the seal-air 16 simply flows out straight in a direction of the height (a radial direction of the turbine) of the moving blade 5 without being squeezed by a nozzle or the like. On the other hand, the moving blade 5 is rotating in a direction of an outline arrow mark together with the rotor 4. Therefore, from the relative relationship between the flow-out of the seal-air 16 and the rotation of the moving blade 5, the seal-air 16 flows at the incidence angle is to the rear-surface side 11 at the front edge 17 of the hub portion of the moving blade 5, as shown in Fig. 17.

As explained above, when the incidence angle is of the seal-air 16 becomes large at the front edge 17 of the hub portion of the moving blade 5 as well, the pressure loss becomes large and the turbine efficiency is lowered by that amount as shown in Fig. 17 and Fig. 18, in a similar manner to that at the front edge 12 of the chip portion of the stationary blade 3.

This problem of the hub portion of the moving blade 5 also applies to a shrouded moving blade in addition to

the above-described free-standing moving blade. In Fig. 17, a reference symbol  $\beta_s$  denotes an entrance metal angle at the hub portion of the moving blade 5. Similarly, a reference symbol  $\theta_s$  denotes a front-edge including angle at the hub portion of the moving blade 5. Similarly, a reference number 24 denotes a camber line for connecting between the front edge 17 of the hub portion of the moving blade 5 and a rear edge 25 of the hub portion.

Further, when the moving blade 5 at a certain stage is a free-standing moving blade, there is the following problem.

Namely, as shown in Fig. 17, the leakage flow 9 is generated from the belly surface 10 side of the moving blade 5 to the rear surface 11 side, at the clearance 8 between the chip 7 of the free-standing moving blade 5 and the casing 1.

Then, as shown in Fig. 19B, a design Mach number distribution shown by a solid-line curve becomes an actual Mach number distribution as shown by a broken-line curve. As a result, on the rear surface 11 of the chip portion 18 of the moving blade 5, deceleration from an intermediate portion to a rear edge 19 is larger in actual Mach distribution G2 than in design Mach distribution G1.

When the deceleration is large, as shown in Fig. 19A, a boundary layer (a portion provided with shaded lines) 20

at a portion from the intermediate portion to the rear edge  
19 swells on the rear surface 11 of the chip portion 18 of  
the moving blade 5. As a result, the pressure loss becomes  
large, and the turbine efficiency is lowered by that amount.  
5 A reference number 21 in Fig. 19 denotes a front edge of  
the chip portion 18 of the moving blade 5.

#### SUMMARY OF THE INVENTION

It is an object of this invention to provide a blade  
10 structure in a gas turbine capable of improving the turbine  
efficiency by minimizing the pressure loss.

In the blade structure in a gas turbine according to  
one aspect of this invention, a front-edge including angle  
at a chip portion of the stationary blade that is the  
15 stationary blade at the rear stage of the moving blade having  
the chip clearance is larger than a front-edge including  
angle at other portions than the chip portion of the  
stationary blade.

According to the above-mentioned aspect, a curve of  
20 a relative relationship between the incidence angle and the  
pressure loss becomes mild by making the front-edge including  
angle large. It is possible to reduce the pressure loss  
by that amount, and therefore, it becomes possible to improve  
the turbine efficiency.

25 In the blade structure in a gas turbine according to

another aspect of this invention, an entrance metal angle at a chip portion of the stationary blade that is the stationary blade at the rear stage of the moving blade having the chip clearance is made smaller than an entrance metal  
5 angle at other portions than the chip portion of the stationary blade.

According to the above-mentioned aspect, it is possible to make the incidence angle small by making the entrance metal angle small. It is possible to reduce the  
10 pressure loss by that amount, and therefore, it becomes possible to improve the turbine efficiency.

In the blade structure in a gas turbine according to still another aspect of this invention, a front-edge including angle at a chip portion of the stationary blade  
15 that is the stationary blade at the rear stage of the moving blade having the chip clearance is made larger than a front-edge including angle at other portions than the chip portion of the stationary blade, and also an entrance metal angle at a chip portion of the stationary blade is made smaller  
20 than an entrance metal angle at other portions than the chip portion of the stationary blade.

According to the above-mentioned aspect, a curve of a relative relationship between the incidence angle and the pressure loss becomes mild by making the front-edge including  
25 angle large. It is possible to reduce the pressure loss

by that amount, and therefore, it becomes possible to improve  
the turbine efficiency. Moreover, it is possible to make  
the incidence angle small by making the entrance metal angle  
small. Also; it is possible to reduce the pressure loss  
5 by that amount, and therefore, it becomes possible to improve  
the turbine efficiency. Moreover, it is possible to make  
the pressure loss much smaller based on a synergy effect  
of the work that a curve of a relative relationship between  
the incidence angle and the pressure loss becomes mild and  
10 the work that the incidence angle can be made small.

In the blade structure in a gas turbine according to  
still another aspect of this invention, a front-edge  
including angle at a hub portion of the stationary blade  
is made larger than a front-edge including angle at other  
15 portions than the hub portion of the moving blade.

According to the above-mentioned aspect, a curve of  
a relative relationship between the incidence angle and the  
pressure loss becomes mild by making the front-edge including  
angle large. It is possible to reduce the pressure loss  
20 by that amount, and therefore, it becomes possible to improve  
the turbine efficiency.

In the blade structure in a gas turbine according to  
still another aspect of this invention, an entrance metal  
angle at a hub portion of the stationary blade is made smaller  
25 than an entrance metal angle at other portions than the hub



portion of the moving blade.

According to the above-mentioned aspect, it is possible to make the incidence angle small by making the entrance metal angle small. It is possible to reduce the pressure loss by that amount, and therefore, it becomes possible to improve the turbine efficiency.

In the blade structure in a gas turbine according to still another aspect of this invention, a front-edge including angle at a hub portion of the stationary blade is made larger than a front-edge including angle at other portions than the hub portion of the moving blade, and also an entrance metal angle at a hub portion of the stationary blade is made smaller than an entrance metal angle at other portions than the hub portion of the moving blade.

According to the above-mentioned aspect, a curve of a relative relationship between the incidence angle and the pressure loss becomes mild by making the front-edge including angle large. It is possible to reduce the pressure loss by that amount, and therefore, it becomes possible to improve the turbine efficiency. Moreover, it is possible to make the incidence angle small by making the entrance metal angle small. It is possible to reduce the pressure loss by that amount, and therefore, it becomes possible to improve the turbine efficiency. Furthermore, it is possible to make the pressure loss much smaller based on a synergy effect

of the work that a curve of a relative relationship between the incidence angle and the pressure loss becomes mild and the work that the incidence angle can be made small.

In the blade structure in a gas turbine according to still another aspect of this invention, a chord length at a chip portion of the moving blade having the chip clearance is made larger than a minimum chord length at other portions than the chip portion of the moving blade.

According to the above-mentioned aspect, it is possible to make small the deceleration from the intermediate portion to the rear edge on the rear surface of the chip portion of the moving blade by making the chord length of the moving blade large. Then, it is possible to minimize the swelling of the boundary layer. As a result, it is possible to make the pressure loss small, and it becomes possible to improve the turbine efficiency by that amount.

Other objects and features of this invention will become apparent from the following description with reference to the accompanying drawings.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is an explanatory diagram of a cross section of a chip portion of a stationary blade showing a first embodiment of a blade structure in a gas turbine according to this invention.

Fig. 2 is an explanatory diagram of a cross section of a chip portion of a stationary blade showing a second embodiment of a blade structure in a gas turbine according to this invention.

5 Fig. 3 is an explanatory diagram of a cross section of a chip portion of a stationary blade showing a third embodiment of a blade structure in a gas turbine according to this invention.

10 Fig. 4 is a perspective view of the stationary blade of the same.

Fig. 5 is an explanatory diagram of a cross section of a hub portion of a moving blade showing a fourth embodiment of a blade structure in a gas turbine according to this invention.

15 Fig. 6 is an explanatory diagram of a cross section of a hub portion of a moving blade showing a fifth embodiment of a blade structure in a gas turbine according to this invention.

20 Fig. 7 is an explanatory diagram of a cross section of a hub portion of a moving blade showing a sixth embodiment of a blade structure in a gas turbine according to this invention.

Fig. 8 is a perspective view of the moving blade of the same.

25 Fig. 9 is an explanatory diagram of a cross section

of a stacking shape of a moving blade showing a seventh embodiment of a blade structure in a gas turbine according to this invention.

Fig. 10 is a diagram of Fig. 9 viewed from a direction of X.

Fig. 11 is a diagram of Fig. 9 viewed from a direction of XI.

Fig. 12A is an explanatory diagram of a cross section of a hub portion of a moving blade showing a chord length, Fig. 12B is an explanatory diagram of a Mach number distribution according the moving blade shown in Fig. 12A.

Fig. 13 is an explanatory diagram showing a modification of the seventh embodiment of a blade structure in a gas turbine according to this invention.

Fig. 14A is an explanatory diagram of a cross section of a moving blade and a stationary blade showing a conventional blade structure, and Fig. 14B is an explanatory diagram of a cross section of a moving blade and a stationary blade showing a modification of the seventh embodiment of a blade structure in a gas turbine according to this invention.

Fig. 15A is an explanatory diagram of a cooling moving blade showing a modification of the seventh embodiment of a blade structure in a gas turbine according to this invention, and Fig. 15B is an explanatory diagram of a moving blade

having a taper according to the same.

Fig. 16 is an explanatory diagram of a moving blade and a stationary blade showing a conventional blade structure.

5 Fig. 17 is an explanatory diagram of a cross section of a moving blade and a stationary blade showing a conventional blade structure.

Fig. 18 is an explanatory diagram showing a relative relationship between an incidence angle and a pressure loss.

10 Fig. 19A is an explanatory diagram of a cross section of a hub portion of a moving blade showing a conventional blade structure, and Fig. 19B is an explanatory diagram of a Mach number distribution according to the moving blade shown in Fig. 19A.

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#### DETAILED DESCRIPTIONS

Embodiments of a blade structure in a gas turbine relating to this invention will be explained below with reference to the accompanying drawings. It should be noted  
20 that the blade structure in the gas turbine is not limited to these embodiments.

Fig. 1 is an explanatory diagram showing a first embodiment of a blade structure in a gas turbine relating to this invention. In the drawing, reference numbers that  
25 are the same as those in Fig. 16 to Fig. 19 show the identical

portions.

A blade structure in a first embodiment relates to a stationary blade 3 at the rear stage of a moving blade having a chip clearance. A front-edge including angle  $\theta_{c1}$  at a front edge of a chip portion (a cross section of a chip) of the stationary blade 3 is made larger than a front-edge including angle of portions (a cross section of a hub portion to a mean portion) other than the chip portion of this stationary blade 3. For example, this is made larger than about  $5^\circ$ .

According to the blade structure of this first embodiment, the front-edge including angle  $\theta_{c1}$  is taken large at the chip portion of the stationary blade 3 at the rear stage of the moving blade having the chip clearance. With this arrangement, a curve of a relative relationship between the incidence angle and the pressure loss becomes mild as shown by a broken-line curve in Fig. 18. As a result, it is possible to make the pressure loss small as shown by a point P3 in Fig. 18. Therefore, it becomes possible to improve the turbine efficiency.

Fig. 2 is an explanatory diagram showing a second embodiment of a blade structure in a gas turbine relating to this invention. In the drawing, reference numbers that are the same as those in Fig. 1 and Fig. 16 to Fig. 19 show the identical portions.

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- A blade structure in a second embodiment relates to a stationary blade 3 at the rear stage of a moving blade having a chip clearance. An entrance metal angle  $\beta_{c1}$  of a chip portion (a cross section of a chip) of this stationary blade 3 is made smaller than an entrance metal angle of portions (a cross section of a hub portion to a mean portion) other than the chip portion of this stationary blade 3. In other words, the entrance metal angle  $\beta_{c1}$  of the cross section of the chip portion of the stationary blade 3 is directed toward a rear surface 13 side by about  $10^\circ$ , for example, as compared with the entrance metal angle of the cross section of the hub portion to the mean portion.

According to the blade structure of this second embodiment, the entrance metal angle  $\beta_{c1}$  is taken small at the chip portion of the stationary blade 3 at the rear stage of the moving blade having the chip clearance. With this arrangement, it is possible to make an incidence angle  $i_{c1}$  small as shown by a point P4 in Fig. 18. As a result, it is possible to make the pressure loss small. Therefore, it becomes possible to improve the turbine efficiency.

Fig. 3 and Fig. 4 are explanatory diagrams showing a third embodiment of a blade structure in a gas turbine relating to this invention. In the drawings, reference numbers that are the same as those in Fig. 1, Fig. 2 and Fig. 16 to Fig. 19 show the identical portions.

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A blade structure in a third embodiment relates to a stationary blade 3 at the rear stage of a moving blade having a chip clearance. A front-edge including angle  $\theta_{c1}$  at a front edge of a chip portion (a cross section of a chip) of the stationary blade 3 is made larger than a front-edge including angle of portions (a cross section of a hub portion to a mean portion) other than the chip portion of this stationary blade 3. For example, this is made larger than about  $5^\circ$ .

Further, an entrance metal angle  $\beta_{c1}$  of a chip portion (a cross section of a chip) of this stationary blade 3 is made smaller than an entrance metal angle of portions (a cross section of a hub portion to a mean portion) other than the chip portion of this stationary blade 3. In other words, the entrance metal angle  $\beta_{c1}$  of the cross section of the chip portion of the stationary blade 3 is directed toward a rear surface 13 side by about  $10^\circ$ , for example, as compared with the entrance metal angle of the cross section of the hub portion to the mean portion.

According to the blade structure of this third embodiment, the front-edge including angle  $\theta_{c1}$  is taken large at the chip portion of the stationary blade 3 at the rear stage of the moving blade having the chip clearance. With this arrangement, a curve of a relative relationship between the incidence angle and the pressure loss becomes mild as



shown by the broken-line curve in Fig. 18. As a result, it is possible to make the pressure loss small as shown by the point P3 in Fig. 18. Therefore, it becomes possible to improve the turbine efficiency.

5 Further, according to the blade structure of this third embodiment, the entrance metal angle  $\beta_{c1}$  is taken small at the chip portion of the stationary blade 3 at the rear stage of the moving blade having the chip clearance. With this arrangement, it is possible to make an incidence angle  $i_{c1}$  10 small as shown by the point P4 in Fig. 18. As a result, it is possible to make the pressure loss small. Therefore, it becomes possible to improve the turbine efficiency.

Particularly, according to the blade structure of this third embodiment, it is possible to make the pressure loss 15 much smaller, based on a synergy effect of the work that a curve of a relative relationship between the incidence angle and the pressure loss becomes mild as shown by the broken-line curve in Fig. 18 and the work that the incidence angle  $i_{c1}$  can be made small as shown by a point P5 in Fig. 20 18. As a result, it becomes possible to improve the turbine efficiency.

Fig. 5 is an explanatory diagram showing a first embodiment of a blade structure in a gas turbine relating to this invention. In the drawing, reference numbers that 25 are the same as those in Fig. 1 to Fig. 4 and Fig. 16 to

Fig. -19 show the identical portions.

A blade structure in a fourth embodiment relates to a moving blade 5 like a free-standing moving blade and a shrouded moving blade. A front-edge including angle  $\theta_{s1}$  at a hub portion (a cross section of a hub portion) of this moving blade 5 is made larger than a front-edge including angle of portions (a cross section of a chip portion to a mean portion) other than the hub portion of this moving blade 5. For example, this is made larger than about  $5^\circ$ .

According to the blade structure of this fourth embodiment, the front-edge including angle  $\theta_{s1}$  is taken large at the hub portion of this moving blade 5. With this arrangement, a curve of a relative relationship between the incidence angle and the pressure loss becomes mild as shown by the broken-line curve in Fig. 18. As a result, it is possible to make the pressure loss small as shown by the point P3 in Fig. 18. Therefore, it becomes possible to improve the turbine efficiency.

Fig. 6 is an explanatory diagram showing a fifth embodiment of a blade structure in a gas turbine relating to this invention. In the drawing, reference numbers that are the same as those in Fig. 1 to Fig. 5 and Fig. 16 to Fig. 19 show the identical portions.

A blade structure in a fifth embodiment relates to a moving blade 5 like a free-standing moving blade and a

shrouded moving blade. An entrance metal angle  $\beta_{s1}$  of a hub portion (a cross section of a hub portion) of this moving blade 5 is made smaller than an entrance metal angle of portions (a cross section of a chip portion to a mean portion) other than the hub portion of this moving blade 5. In other words, the entrance metal angle  $\beta_{s1}$  of the cross section of the hub portion of the moving blade 5 is directed toward a rear surface 11 side by about  $10^\circ$ , for example, as compared with the entrance metal angle of the cross section of the chip portion to the mean portion.

According to the blade structure of this fifth embodiment, the entrance metal angle  $\beta_{s1}$  is taken small at the hub portion of the moving blade 5. With this arrangement, it is possible to make an incidence angle  $i_{s1}$  small as shown by the point P4 in Fig. 18. As a result, it is possible to make the pressure loss small. Therefore, it becomes possible to improve the turbine efficiency.

Fig. 7 and Fig. 8 are explanatory diagrams showing a sixth embodiment of a blade structure in a gas turbine relating to this invention. In the drawings, reference numbers that are the same as those in Fig. 1 to Fig. 6 and Fig. 16 to Fig. 19 show the identical portions.

A blade structure in a sixth embodiment relates to a moving blade 5 like a free-standing moving blade and a shrouded moving blade. A front-edge including angle  $\theta_{s1}$

at a hub portion (a cross section of a hub portion) of this moving blade 5 is made larger than a front-edge including angle of portions (a cross section of a chip portion to a mean portion) other than the hub portion of this moving blade 5. For example, this is made larger than about  $5^\circ$ .

Further, an entrance metal angle  $\beta_{s1}$  of a hub portion (a cross section of a hub portion) of this moving blade 5 is made smaller than an entrance metal angle of portions (a cross section of a chip portion to a mean portion) other than the hub portion of this moving blade 5. In other words, the entrance metal angle  $\beta_{s1}$  of the cross section of the hub portion of the moving blade 5 is directed toward a rear surface 11 side by about  $10^\circ$ , for example, as compared with the entrance metal angle of the cross section of the chip portion to the mean portion.

According to the blade structure of this sixth embodiment, the front-edge including angle  $\theta_{s1}$  is taken large at the hub portion of this moving blade 5. With this arrangement, a curve of a relative relationship between the incidence angle and the pressure loss becomes mild as shown by the broken-line curve in Fig. 18. As a result, it is possible to make the pressure loss small as shown by the point P3 in Fig. 18. Therefore, it becomes possible to improve the turbine efficiency.

Further, according to the blade structure of this sixth

embodiment, the entrance metal angle  $\beta_{s1}$  is taken small at the hub portion of the moving blade 5. With this arrangement, it is possible to make an incidence angle  $i_{s1}$  small as shown by the point-P4 in Fig. 18. As a result, it is possible to make the pressure loss small. Therefore, it becomes possible to improve the turbine efficiency.

Particularly, according to the blade structure of this sixth embodiment, it is possible to make the pressure loss much smaller, based on a synergy effect of the work that a curve of a relative relationship between the incidence angle and the pressure loss becomes mild as shown by the broken-line curve in Fig. 18 and the work that the incidence angle  $i_{s1}$  can be made small as shown by the point P5 in Fig. 18. As a result, it becomes possible to improve the turbine efficiency.

Fig. 9 and Fig. 12 are explanatory diagrams showing a seventh embodiment of a blade structure in a gas turbine relating to this invention. In the drawings, reference numbers that are the same as those in Fig. 1 to Fig. 8 and Fig. 16 to Fig. 19 show the identical portions.

A blade structure in a seventh embodiment relates to a moving blade 5 like a free-standing moving blade and a shrouded moving blade. A chord length 26 at a chip portion 18 (a cross section of the chip portion 18) of this moving blade 5 is made larger than a minimum chord length at other

portions (a cross section of a hub portion to a mean section) than the chip portion of the moving blade 5. In other words, the chord length 26 of the cross section of the chip portion 18 is made equal to or larger than the chord length of the mean cross section (a ratio of pitch to chord is set larger than a conventional ratio).

Fig. 9 is an explanatory diagram of a cross section showing a stacking shape of the moving blade 5. In Fig. 9 to Fig. 11, a stacking shape shown by a reference number 50 and a solid line show a chip. A stacking shape shown by a reference number 51 and a one-dot chained line show a chip at a position of about 75% of the height from a hub. Further, a stacking shape shown by a reference number 52 and a two-dot chained line show a mean. Further, a stacking shape shown by a reference number 53 and a three-dot chained line show a chip at a position of about 25% of the height from the hub. Last, a stacking shape shown by a reference number 54 and a broken line show the hub.

According to the blade structure of this sixth embodiment, it is possible to make small the deceleration from an intermediate portion to a rear edge 19 on a rear surface 11 of a chip portion 18 of a moving blade 5, as shown by G4 in Fig. 12B, by making large a chord length 26 of the chip portion 18 of the moving blade 5.

Namely, in Mach number distributions in Fig. 12B and

Fig. 19B, an area of a portion encircled by a solid-line curve (an area of a portion provided with shaded lines, and a pressure difference)  $S$  is constant. In this case, when the chord length 26 of the chip portion 18 of the moving blade 5 is made large, the area  $S$  of the Mach number distribution changes from a vertically-long shape shown in Fig. 19B to a laterally-long shape shown in Fig. 12B. As a result, the deceleration changes from  $G2$  shown in Fig. 19B to small  $G4$  shown in Fig. 12B. Consequently, it is possible to restrict the swelling of the boundary layer. Therefore, it is possible to make the pressure loss small, and it becomes possible to improve the turbine efficiency by that amount.

Fig. 13 to Fig. 15 show modifications of a blade structure in a gas turbine relating to this invention. In these drawings, reference numbers that are the same as those in Fig. 1 to Fig. 12 and Fig. 16 to Fig. 19 show the identical portions.

First, a modification shown in Fig. 13 is a modification of the seventh embodiment. Chip portions of stationary blades 2 and 3 are provided with escape sections 27 for avoiding an interference with a chip portion 18 of a moving blade 5.

According to this seventh embodiment, there is no room for mutual interference between the chip portion 18 of the

moving blade 5 and the chip portions of the stationary blades  
2 and 3 adjacent to each other, even when the chord length  
26 of the chip portion 18 of the moving blade 5 is made large.  
A two-dot chained line in Fig. 13 shows a conventional blade  
5 structure.

Next, a modification shown in Fig. 14B is a modification  
of the seventh embodiment. As an escape section of the chip  
portion of the stationary blade 3, the entrance metal angle  
 $\beta_{c1}$  of the chip portion of the stationary blade 3 is made  
10 smaller than the entrance metal angle of portions (the hub  
portion to the mean portion) other than the chip portion  
of the stationary blade 3. In other words, as shown in Fig.  
2, Fig. 3 and Fig. 4, the entrance metal angle  $\beta_{c1}$  of the  
chip portion of the stationary blade 3 is directed toward  
15 the rear surface 13 side of the stationary blade 3. It is  
also possible to have a similar structure for the stationary  
blade 2 at the same stage as that of the moving blade 5.

According to the modification shown in this Fig. 14B,  
as the entrance metal angle  $\beta_{c1}$  of the chip portion of the  
20 stationary blade 3 is directed toward the rear surface 13  
side of the stationary blade 3, it is possible to have a  
width  $W1$  in an axial direction of the stationary blade 3  
smaller than a width  $W2$  of a conventional moving blade shown  
in Fig. 14A. As a result, even when a width  $W3$  in the axial  
25 direction of the moving blade 5 is made larger than a



conventional width W4 by increasing the chord length 26 of the chip portion 18 of the moving blade 5, a width W5 from the moving blade 5 to the stationary blade 3 makes little change from a conventional width W6. Therefore, there is  
5 no room for mutual interference between the chip portion 18 of the moving blade 5 and the chip portion of the stationary blade 3 adjacent to each other, even when the chord length 26 of the chip portion 18 of the moving blade 5 is made large.

Further, according to the modification shown in this  
10 Fig. 14B, as the entrance metal angle  $\beta_{c1}$  of the chip portion of the stationary blade 3 is smaller than the entrance metal angle of the hub portion to the mean portion other than the chip portion of the stationary blade 3, it becomes possible to make the incidence angle  $i_{c1}$  small as shown by the point  
15 P4 in Fig. 18. As it is possible to make the pressure loss smaller by that amount, it becomes possible to improve the turbine efficiency.

Then, the blade structure relating to this invention can also be applied to a cooling moving blade 29 having a  
20 hollow portion 28 at the chip portion 18, as shown in Fig. 15A. Further, it is also possible to apply the blade structure relating to this invention to a moving blade 31 of which chip portion 18 has a taper 30 along the taper of the casing 1, as shown in Fig. 15B.

25 As is clear from the above, according to the blade

structure in a gas turbine relating to one aspect of this invention, a front-edge including angle is taken large, at a chip portion of a stationary blade at a rear stage of a moving blade having a chip clearance. Therefore, a curve  
5 of a relative relationship between the incidence angle and the pressure loss becomes mild. As it is possible to reduce the pressure loss by that amount, it becomes possible to improve the turbine efficiency.

According to the blade structure in a gas turbine  
10 relating to another aspect of this invention, it is possible to make an incidence angle small by making an entrance metal angle small, at a chip portion of a stationary blade at a rear stage of a moving blade having a clearance. As it is possible to reduce the pressure loss by that amount, it  
15 becomes possible to improve the turbine efficiency.

According to the blade structure in a gas turbine relating to still another aspect of this invention, a front-edge including angle is taken large at a chip portion of a stationary blade, at a rear stage of a moving blade  
20 having a chip clearance. Therefore, a curve of a relative relationship between an incidence angle and a pressure loss becomes mild. As it is possible to reduce the pressure loss by that amount, it becomes possible to improve the turbine efficiency.

25 According to the blade structure in a gas turbine

relating to still another aspect of this invention, it is possible to make an incidence angle small by making an entrance metal angle small, at a chip portion of a stationary blade at a rear stage of a moving blade having a clearance.

5 As it is possible to reduce the pressure loss by that amount, it becomes possible to improve the turbine efficiency.

According to the blade structure in a gas turbine relating to still another aspect of this invention, it is possible to make the pressure loss much smaller based on

10 a synergy effect of the work that a curve of a relative relationship between an incidence angle and a pressure loss becomes mild and the work that the incidence angle can be made small. As a result, it becomes possible to improve the turbine efficiency.

15 According to the blade structure in a gas turbine relating to still another aspect of this invention, a curve of a relative relationship between an incidence angle and a pressure loss becomes mild by making a front-edge including angle large at a hub portion of a moving blade. As it is

20 possible to reduce the pressure loss by that amount, it becomes possible to improve the turbine efficiency.

According to the blade structure in a gas turbine relating to still another aspect of this invention, it is possible to make an incidence angle small by making an

25 entrance metal angle small at a hub portion of a moving blade.

As it is possible to reduce the pressure loss by that amount,  
it becomes possible to improve the turbine efficiency.

According to the blade structure in a gas turbine  
relating to still another aspect of this invention, a curve  
5 of a relative relationship between an incidence angle and  
a pressure loss becomes mild by making a front-edge including  
angle large at a hub portion of a moving blade. As it is  
possible to reduce the pressure loss by that amount, it  
becomes possible to improve the turbine efficiency.

10 According to the blade structure in a gas turbine  
relating to still another aspect of this invention, it is  
possible to make an incidence angle small by making an  
entrance metal angle small at a hub portion of a moving blade.  
As it is possible to reduce the pressure loss by that amount,  
15 it becomes possible to improve the turbine efficiency.

According to the blade structure in a gas turbine  
relating to still another aspect of this invention, it is  
possible to make the pressure loss much smaller based on  
a synergy effect of the work that a curve of a relative  
20 relationship between an incidence angle and a pressure loss  
becomes mild and the work that the incidence angle can be  
made small. As a result, it becomes possible to improve  
the turbine efficiency.

According to the blade structure in a gas turbine  
25 relating to still another aspect of this invention, it is

possible to make small the deceleration from an intermediate portion to a rear edge on a rear surface of a chip portion of a moving blade by making a chord length of the moving blade large. Then, it is possible to minimize the swelling of the boundary layer. As a result, it is possible to make the pressure loss small, and it becomes possible to improve the turbine efficiency by that amount.

Furthermore, a chip portion of a stationary blade is provided with an escape section for avoiding an interference with a chip portion of a moving blade. As a result, there is no room for mutual interference between a chip portion of the moving blade and chip portions of stationary blades adjacent to each other, even when a chord length of the chip portion of the moving blade is made large.

Moreover, as an entrance metal angle at a chip portion of a stationary blade is directed toward the rear surface side of the stationary blade, there is no room for mutual interference between a chip portion of a moving blade and chip portions of stationary blades adjacent to each other, even when the chord length of the chip portion of the moving blade is made large.

Furthermore, as an entrance metal angle at a chip portion of a stationary blade is smaller than an entrance metal angle at other portions than the chip portion of the stationary blade, it is possible to make an incidence angle

small. As it is possible to reduce the pressure loss by that amount, it becomes possible to improve the turbine efficiency.

Although the invention has been described with respect  
5 to a specific embodiment for a complete and clear disclosure,  
the appended claims are not to be thus limited but are to  
be construed as embodying all modifications and alternative  
constructions that may occur to one skilled in the art which  
fairly fall within the basic teaching herein set forth.

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